

Experimental Determination of the Vapor–Liquid Equilibrium at 101.32 kPa of the Ternary System 1-Butanol + Methanol + TAME

Alberto Arce,* Eva Rodil, and Ana Soto

Department of Chemical Engineering, University of Santiago de Compostela, E-15706 Santiago, Spain

Experimental isobaric vapor–liquid equilibrium data are reported at 101.32 kPa for the ternary system 1-butanol + methanol + TAME (2-methoxy-2-methylbutane or *tert*-amyl methyl ether) and for one unmeasured constituent binary system (TAME + 1-butanol). These data were found to be thermodynamically consistent and were satisfactorily correlated with the Wilson, NRTL, and UNIQUAC equations. They have also been compared with predictions obtained from the application of ASOG and UNIFAC group contribution methods and from the correlation equations using interaction parameters of the constituent binary systems.

Introduction

In previous work^{1,2} we have demonstrated that 1-butanol is a possible entrainer for the separation of MTBE (methyl *tert*-butyl ether) and methanol or ethanol by extractive distillation. To know if the same entrainer can be used in the separation of methanol + TAME (2-methoxy-2-methylbutane or *tert*-amyl methyl ether) mixtures, a rigorous determination of the involved ternary equilibrium is necessary. With this in mind, isobaric ($P = 101.32$ kPa) vapor–liquid equilibrium (VLE) data for the system 1-butanol + methanol + TAME will be determined and fitted with the equations of Wilson,³ NRTL,⁴ and UNIQUAC.⁵ The prediction of equilibrium will also be tested, first using the Wilson, NRTL, and UNIQUAC equations with the interaction parameters of the corresponding binary systems, and then by the group contribution methods ASOG-KT,^{6,7} UNIFAC,⁸ UNIFAC–Dortmund,^{9,10} and UNIFAC–Lyngby.¹¹

Experimental Section

Materials. Methanol was supplied by Merck with nominal purity >99.8 mass %. 1-Butanol was supplied by Aldrich with nominal purity >99.9 mass %, and TAME was supplied by Fluka with nominal purity >98.9 mass %. The water contents of the methanol, 1-butanol, and TAME (determined with a Metrohm 737 KF coulometer) were 0.03, 0.1, and 0.02 mass %, respectively.

Table 1 lists the densities and refractive indices at 298.15 K and atmospheric pressure and boiling points at 101.32 kPa measured for the pure components, together with published values for these parameters.^{12–14}

Apparatus and Procedure. The VLE experiments in this study were performed using a dynamic recirculating still equipped with a Cottrell pump. It is a commercial unit (Labodest model 602), built by Fischer, capable of handling pressures from 0.25 to 400 kPa and temperatures up to 513.15 K. The temperature was measured using a Heraeus QuaT100 quartz thermometer, with an accuracy of ± 0.02 K, and pressure was measured with a Fischer digital manometer with an accuracy of ± 0.01 kPa.

Distillation was performed under an inert argon atmosphere at constant pressure of 101.32 kPa, and the heating and stirring system of the liquid mixture was connected.

Table 1. Densities, ρ , Refractive Indices, n_D , and Boiling Points, T_b , of the Pure Components

com- ponent	$\rho(298.15\text{ K}), \text{g}\cdot\text{cm}^{-3}$		$n_D(298.15\text{ K})$		$T_b(101.32\text{ kPa}), \text{K}$	
	exptl	lit.	exptl	lit.	exptl	lit.
1-butanol	0.8060	0.80575 ^a	1.3975	1.39741 ^a	390.88	390.875 ^a
methanol	0.7866	0.78637 ^a	1.3264	1.32652 ^a	337.65	337.696 ^a
TAME	0.7658	0.76577 ^b	1.3858	1.38580 ^b	359.33	359.39 ^c

^a Riddick et al.¹² ^b Linek.¹³ ^c Krähenbühl and Gmehling.¹⁴

Table 2. Isobaric Vapor–Liquid Equilibrium Data for the TAME (1) + 1-Butanol (2) Binary System at 101.32 kPa

T/K	$x_1/(\text{mole fraction})$	$y_1/(\text{mole fraction})$	γ_1	γ_2
387.99	0.0279	0.0988	1.7434	1.0245
386.33	0.0508	0.1646	1.6551	1.0313
384.79	0.0763	0.2344	1.6241	1.0263
382.60	0.1118	0.3232	1.6066	1.0221
380.90	0.1395	0.3897	1.6151	1.0133
378.46	0.1897	0.4691	1.5152	1.0265
377.05	0.2170	0.5142	1.5024	1.0262
374.78	0.2715	0.5826	1.4387	1.0356
372.96	0.3183	0.6339	1.3975	1.0435
371.41	0.3577	0.6830	1.3939	1.0216
369.70	0.4169	0.7296	1.3347	1.0293
367.90	0.4816	0.7709	1.2797	1.0571
366.16	0.5648	0.8093	1.1997	1.1280
364.30	0.6571	0.8495	1.1381	1.2236
362.84	0.7503	0.8838	1.0791	1.3829
361.91	0.8143	0.9054	1.0450	1.5774
360.92	0.8911	0.9382	1.0171	1.8381
360.13	0.9382	0.9621	1.0157	2.0683

The system was kept at boiling point for 20 min to ensure the stationary state, and then we extracted samples of liquid and vapor with syringes. The composition of liquid and vapor samples for the binary and ternary mixtures was determined by measuring their densities at 298.15 K with an Anton Paar DSA-48 vibrating tube densimeter and sound analyzer, and refractive indices were determined with an Atago RX-1000 refractometer at 298.15 K. The composition dependence of densities and refractive indices has previously been reported.¹⁵ The greatest uncertainty found for these systems with this method of composition analysis was ± 0.003 in mole fraction.

Table 3. Isobaric Vapor–Liquid Equilibrium Data for the 1-Butanol (1) + Methanol (2) + TAME (3) Ternary System at 101.32 kPa

T/K	x_1	x_2	y_1	y_2	γ_1	γ_2	γ_3	T/K	x_1	x_2	y_1	y_2	γ_1	γ_2	γ_3
338.63	0.1211	0.7060	0.0116	0.7870	0.8667	1.0792	2.3010	357.89	0.2787	0.0513	0.1003	0.2003	1.3143	1.9606	1.1024
338.69	0.1241	0.6640	0.0140	0.7600	1.0173	1.1063	2.0976	358.09	0.3855	0.0770	0.1099	0.2746	1.0287	1.7706	1.2051
338.82	0.1261	0.7449	0.0126	0.8213	0.8955	1.0590	2.5358	358.32	0.4308	0.1056	0.1198	0.3105	0.9917	1.4455	1.2865
338.88	0.1262	0.6079	0.0140	0.7296	0.9908	1.1529	1.8793	358.33	0.0221	0.0064	0.0099	0.0534	1.6268	4.1902	1.0023
338.94	0.1190	0.7893	0.0118	0.8583	0.8837	1.0391	2.7888	358.42	0.0725	0.0082	0.0374	0.0770	1.8594	4.6858	0.9992
339.33	0.1195	0.8209	0.0121	0.8946	0.8851	1.0259	3.0532	358.42	0.4646	0.1148	0.1274	0.3295	0.9727	1.4047	1.3492
339.66	0.1452	0.5440	0.0172	0.6990	1.0166	1.2000	1.7298	358.46	0.4980	0.1234	0.1346	0.3641	0.9559	1.4395	1.3840
339.82	0.1217	0.8500	0.0132	0.9368	0.9255	1.0184	3.4053	358.46	0.5723	0.1524	0.1474	0.4560	0.9088	1.4539	1.5125
340.27	0.1195	0.8698	0.0125	0.9699	0.8732	1.0132	3.1341	358.95	0.6078	0.1699	0.1551	0.5020	0.8806	1.4103	1.6010
340.41	0.1512	0.4706	0.0213	0.6611	1.1640	1.2775	1.5474	359.55	0.0847	0.0144	0.0492	0.0380	1.9949	1.2711	1.0175
340.60	0.1340	0.8548	0.0127	0.9666	0.7780	1.0150	3.4816	359.56	0.4375	0.0724	0.1302	0.2610	1.0064	1.7050	1.2537
341.31	0.1657	0.8198	0.0183	0.9544	0.8744	1.0181	3.4605	359.70	0.6383	0.1872	0.1669	0.5537	0.8728	1.3751	1.6319
341.36	0.1534	0.3928	0.0228	0.6190	1.1713	1.3858	1.4055	359.78	0.1443	0.0193	0.0698	0.0555	1.6406	1.3714	1.0437
341.78	0.1829	0.8002	0.0191	0.9495	0.8075	1.0200	3.3605	359.90	0.2234	0.0247	0.0793	0.1051	1.1939	2.0131	1.0796
343.18	0.1681	0.2956	0.0257	0.5718	1.1013	1.5944	1.2558	360.88	0.6655	0.1978	0.1648	0.5819	0.7858	1.3153	1.8288
343.51	0.2531	0.7189	0.0288	0.9284	0.8069	1.0424	2.6079	361.18	0.2779	0.0254	0.1016	0.0927	1.1624	1.6552	1.1104
344.14	0.1622	0.2584	0.0287	0.5382	1.2164	1.6603	2.1205	362.11	0.4535	0.0442	0.1606	0.1795	1.0745	1.7732	1.2324
344.42	0.3033	0.5958	0.0343	0.8280	0.7655	1.0866	2.2395	362.19	0.6802	0.1903	0.2014	0.5680	0.8876	1.2791	1.6953
344.81	0.2997	0.6671	0.0391	0.9093	0.8674	1.0500	2.5391	362.27	0.3337	0.0126	0.1155	0.0778	1.0501	2.7035	1.1494
344.89	0.3205	0.5563	0.0400	0.7990	0.8252	1.1047	2.1077	362.41	0.3752	0.0171	0.1178	0.1155	0.9452	2.9365	1.1712
345.50	0.1544	0.2075	0.0304	0.4968	1.2678	1.8207	1.1465	362.60	0.4143	0.0271	0.1224	0.1501	0.8808	2.3877	1.2035
345.83	0.3437	0.5170	0.0458	0.7654	0.8415	1.1016	2.1159	363.23	0.4883	0.0427	0.1746	0.1830	1.0338	1.8036	1.2461
346.17	0.3431	0.6170	0.0454	0.8922	0.8233	1.0611	2.4427	363.98	0.5280	0.0445	0.1861	0.2242	0.9857	2.0648	1.2309
346.54	0.3612	0.4722	0.0502	0.7343	0.8479	1.1289	1.9700	364.90	0.7269	0.1797	0.2418	0.5806	0.8894	1.2694	1.6831
346.90	0.3675	0.4390	0.0516	0.7055	0.8419	1.1527	1.8861	365.71	0.5569	0.0568	0.2350	0.1115	1.0994	0.7647	1.4375
347.30	0.1450	0.1509	0.0328	0.4411	1.3376	2.0902	1.0898	367.59	0.5985	0.0551	0.2576	0.1164	1.0369	0.7749	1.4606
347.30	0.3710	0.3993	0.0530	0.6715	0.8404	1.1903	1.7752	368.10	0.7440	0.1038	0.2839	0.3980	0.8947	1.3683	1.6831
347.83	0.3966	0.5561	0.0522	0.8715	0.7560	1.0845	2.3867	368.53	0.7794	0.1503	0.3112	0.5359	0.9191	1.2514	1.7452
348.19	0.1856	0.1254	0.0325	0.4408	0.9925	2.4355	1.0845	368.86	0.6213	0.0573	0.2719	0.1182	1.0008	0.7270	1.4831
348.31	0.3839	0.3509	0.0565	0.6356	0.8253	1.2385	1.6612	369.02	0.7714	0.1202	0.3058	0.4547	0.8949	1.3099	1.7420
349.10	0.3938	0.3034	0.0603	0.5980	0.8273	1.3123	1.5720	369.74	0.6424	0.0544	0.2755	0.1374	0.9461	0.8654	1.4793
349.34	0.1438	0.0941	0.0350	0.3837	1.3087	2.7213	1.0421	369.95	0.7888	0.1407	0.3346	0.5177	0.9221	1.2365	1.6185
349.50	0.4417	0.5078	0.0625	0.8495	0.7507	1.0921	2.4438	371.15	0.6937	0.0102	0.3047	0.1272	0.9153	4.0909	1.4130
350.11	0.1365	0.1136	0.0384	0.3620	1.4596	2.0724	1.0662	373.39	0.7394	0.0103	0.3656	0.0981	0.9423	2.9189	1.4901
350.31	0.3877	0.2655	0.0677	0.5510	0.8917	1.3267	1.4721	373.53	0.7791	0.0269	0.3344	0.2461	0.8120	2.7779	1.5033
350.47	0.3788	0.2365	0.0659	0.5262	0.8823	1.4159	1.4106	373.70	0.7616	0.0157	0.3585	0.1545	0.8855	2.9816	1.5106
351.66	0.1118	0.0840	0.0440	0.3019	1.9034	2.2220	1.0329	375.71	0.8125	0.0216	0.4073	0.1953	0.8710	2.5744	1.5759
351.78	0.3615	0.2219	0.0732	0.4790	0.9669	1.3152	1.3713	376.44	0.8524	0.1042	0.5000	0.3744	0.9885	0.9961	1.8887
352.60	0.0987	0.0685	0.0457	0.2585	2.1479	2.2645	1.0303	376.79	0.8600	0.0800	0.4970	0.3530	0.9611	1.2112	1.6153
353.74	0.3519	0.1836	0.0795	0.4099	0.9876	1.2756	1.3186	376.86	0.8361	0.0277	0.5021	0.1330	0.9976	1.3226	1.7139
354.06	0.5356	0.3875	0.1086	0.7631	0.8701	1.1003	2.0272	377.71	0.8753	0.0557	0.5173	0.2934	0.9492	1.4091	1.7288
354.40	0.0934	0.0441	0.0366	0.2187	1.6787	2.8062	1.0083	377.81	0.8785	0.0916	0.5299	0.3959	0.9651	1.1507	1.5679
354.60	0.2925	0.1025	0.0738	0.3230	1.0640	1.7568	1.1619	378.93	0.8641	0.0236	0.5548	0.1232	0.9859	1.3533	1.7440
355.18	0.5638	0.3443	0.1199	0.7260	0.8672	1.1350	1.9664	379.06	0.8935	0.0671	0.5725	0.3081	0.9779	1.1806	1.8514
356.01	0.5818	0.3100	0.1297	0.6915	0.8756	1.1684	1.8873	380.15	0.8837	0.0280	0.5952	0.1379	0.9877	1.2316	1.7870
356.87	0.5057	0.1393	0.1053	0.4583	0.7894	1.6867	1.3493	380.98	0.9017	0.0394	0.6358	0.1804	1.0022	1.1167	1.8130
357.05	0.5402	0.1526	0.1245	0.4631	0.8659	1.5455	1.4672	382.62	0.9110	0.0235	0.6746	0.1159	0.9914	1.1495	1.7835
357.35	0.3774	0.0911	0.1028	0.2951	1.0151	1.6470	1.2184	382.91	0.9344	0.0571	0.6983	0.2906	0.9897	1.1728	0.7288

Results

The VLE data and the activity coefficients for TAME + 1-butanol and for ternary mixtures at 101.32 kPa are shown in Tables 2 and 3, respectively. Results for the binary mixtures methanol + TAME and methanol + 1-butanol have been given in previous works.^{2,16} Thermodynamic consistency of data has been demonstrated. Binary data passed both Fredenslund's test⁸ (median deviation between calculated and experimental $y_i < 0.01$) and Wisniak's L–W test¹⁷ ($D < 3$), and the ternary data passed both Wisniak's L–W test¹⁷ of thermodynamic consistency ($0.92 < L_i/W_i < 1.08$ at all data points) and Wisniak and Tamir's modification¹⁸ of the test of McDermott–Ellis¹⁹ ($D < D_{\max}$ at all data points). Figure 1 shows the isotherms of the liquid phase for the ternary system.

Data Treatment

Correlation. All data processing was performed using the program ChemCAD IV. For the ternary system and each binary system, the binary interaction parameters of the Wilson, NRTL, and UNIQUAC equations for activity

coefficients were optimized by means of a simplex method for the minimum mean squared deviation between calculated and experimental liquid-phase mole fractions,

$$F = \sum_{i=1}^N (x_{i,\text{calc}} - x_{i,\text{exp}})^2 \quad (1)$$

the calculated values being obtained from the equilibrium equations

$$y_i \phi_i P = x_{i,\text{vap}} P^S \phi_i^S \exp[\nu_{i,\text{L}}^L (P - P^S)/RT] \quad (2)$$

where $P = 101.32$ kPa, x_i and y_i are the mole fractions of component i in the liquid and vapor phases respectively, γ_i is its activity coefficient, $\nu_{i,\text{L}}^L$ is its molar volume in the liquid phase, ϕ_i and ϕ_i^S are its fugacity coefficients under unsaturated and saturated conditions, respectively, and P^S is its vapor pressure at saturation; vapor pressures and liquid-phase molar volumes were calculated using data contained in the ChemCAD IV database, and the fugacity coefficients using the Soave–Redlich–Kwong equation. The

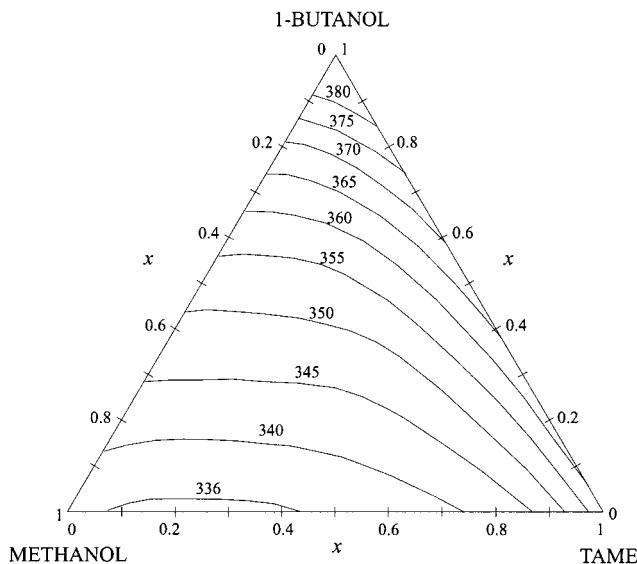


Figure 1. Isothermal liquid-phase compositions of 1-butanol + methanol + TAME at equilibrium with its vapor at 101.32 kPa (temperatures in K).

Table 4. Binary Interaction Parameters ($J \cdot mol^{-1}$) of the Wilson, NRTL, and UNIQUAC Equations As Obtained by Correlating the VLE Data for the Binary Systems, Together with rms Deviations in Equilibrium Temperature and Vapor-Phase Composition

model	parameters	rms T/K	rms y_1
Methanol (1) + TAME (2)			
Wilson	$\Delta\lambda_{12} = 5206.2$, $\Delta\lambda_{21} = -612.91$	0.25	0.0084
UNIQUAC	$\Delta u_{12} = -611.36$, $\Delta u_{21} = 4002.4$	0.26	0.0088
NRTL ($\alpha = 0.3$)	$\Delta g_{12} = 2640.5$, $\Delta g_{21} = 1499.1$	0.26	0.0113
Methanol (1) + 1-Butanol (2)			
Wilson	$\Delta\lambda_{12} = 560.61$, $\Delta\lambda_{21} = 673.66$	0.54	0.0127
UNIQUAC	$\Delta u_{12} = 783.33$, $\Delta u_{21} = -176.06$	0.66	0.0113
NRTL ($\alpha = 0.3$)	$\Delta g_{12} = 258.31$, $\Delta g_{21} = -88.960$	0.56	0.0132
TAME (1) + 1-Butanol (2)			
Wilson	$\Delta\lambda_{12} = -1797.2$, $\Delta\lambda_{21} = 4850.5$	0.44	0.0052
UNIQUAC	$\Delta u_{12} = 2581.5$, $\Delta u_{21} = -1337.3$	0.38	0.0063
NRTL ($\alpha = 0.3$)	$\Delta g_{12} = 3955.4$, $\Delta g_{21} = -1121.6$	0.42	0.0057

optimal value of the NRTL nonrandomness parameter α was found by trial and error to be 0.3 in all cases.

The results for the binary systems are listed in Table 4, and those for the ternary system in Table 5. For the binary systems TAME + methanol¹⁶ and TAME + 1-butanol, a well-defined unique optimal pair of binary interaction parameters was found for each of the fitted equations. However, the parameter pairs listed in Table 4 for methanol + 1-butanol² only provided a slightly better fit than virtually any other parameter pairs in the region explored.

Figure 2 compares, for the ternary system, the calculated values using the NRTL equation ($\alpha = 0.3$) with the experimental VLE data (for the sake of clarity, the number of data points shown has been reduced).

Table 5. Binary Interaction Parameters ($J \cdot mol^{-1}$) of the Wilson, NRTL, and UNIQUAC Equations As Obtained by Correlating the VLE Data for the 1-Butanol (1) + Methanol (2) + TAME (3) Ternary System, Together with rms Deviations in Equilibrium Temperature and Vapor-Phase Composition

model	parameters ($J \cdot mol^{-1}$)	rms T	rms y_1	rms y_2	rms y_3
Wilson	$\Delta\lambda_{12} = -579.78$, $\Delta\lambda_{13} = 4306.6$ $\Delta\lambda_{21} = 1590.63$, $\Delta\lambda_{23} = 5816.6$ $\Delta\lambda_{31} = -1528.87$, $\Delta\lambda_{32} = -1258.1$	0.94	0.0228	0.0341	0.0199
UNIQUAC	$\Delta u_{12} = 1593.5$, $\Delta u_{13} = -1334.8$ $\Delta u_{21} = -583.58$, $\Delta u_{23} = -520.49$ $\Delta u_{31} = 2603.2$, $\Delta u_{32} = 3932.9$	0.94	0.0225	0.0339	0.0197
NRTL ($\alpha = 0.3$)	$\Delta g_{12} = -1499.5$, $\Delta g_{13} = -1040.7$ $\Delta g_{21} = 2593.9$, $\Delta g_{23} = 2686.8$ $\Delta g_{31} = 3831.7$, $\Delta g_{32} = 1489.3$	0.93	0.0229	0.0342	0.0196

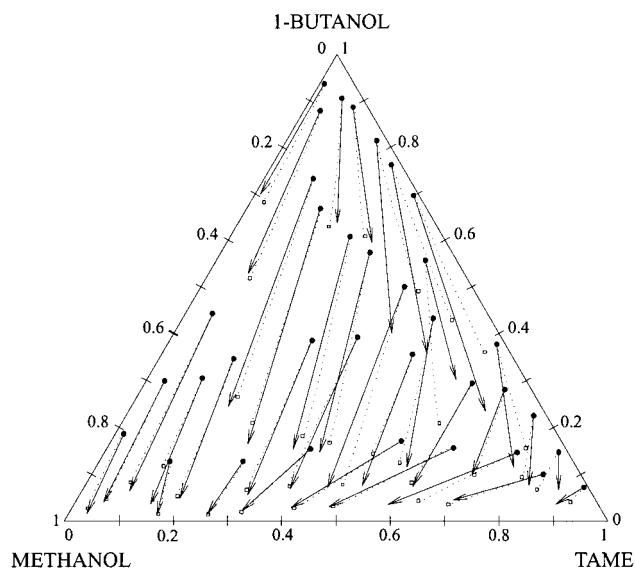


Figure 2. Comparison of the experimental VLE data (—○—) for 1-butanol + methanol + TAME with calculated values using the NRTL ($\alpha = 0.3$) equations (---□---).

Table 6. Root Mean Square Deviations in Equilibrium Temperature and Vapor-Phase Composition of VLE Predictions for TAME + 1-Butanol Obtained by Group Contribution Methods

model	rms T/K	rms y_1
ASOG	0.23	0.0109
UNIFAC	0.41	0.0146
UNIFAC-Dortmund	0.91	0.0230
UNIFAC-Lyngby	0.33	0.0147

Prediction. VLE data for the binary system TAME + 1-butanol were predicted using the following group contribution methods to calculate the liquid-phase activity coefficients: the ASOG-KT method; the original UNIFAC method, with the structural and group-interaction parameters recommended by Gmehling et al.;²⁰ the UNIFAC-Dortmund method; and the UNIFAC-Lyngby method. Table 6 lists the rms deviations between the experimental VLE data and those predicted. Figure 3 shows the vapor-liquid equilibrium composition of the binary system TAME + 1-butanol, comparing the correlation result with the NRTL ($\alpha = 0.3$) equation and prediction with the ASOG-KT method.

For the ternary system, 1-butanol + methanol + TAME, calculations were carried out by means of two methods. Using the group contribution methods cited above along with ternary equations of Wilson, NRTL, and UNIQUAC, models were constructed with the binary interaction parameters of the constituent binary systems (Table 4). Table 7 lists the rms deviations between the experimental VLE data and those predicted by both methods.

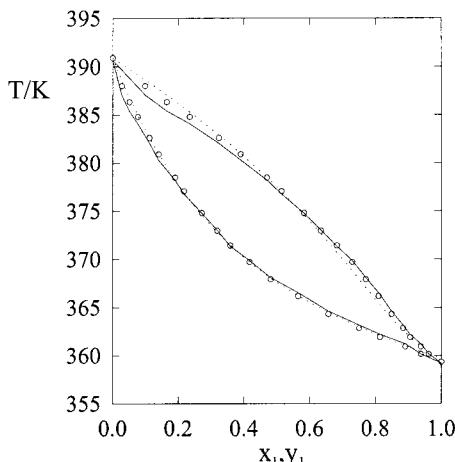


Figure 3. Vapor–liquid equilibrium compositions of TAME + 1-butanol at 101.32 kPa: ○, experimental; —, NRTL ($\alpha = 0.3$) equation; ···, ASOG method.

Table 7. Root Mean Square Deviations in Equilibrium Temperature and Vapor-Phase Composition of VLE Predictions for 1-Butanol (1) + Methanol (2) + TAME (3) Obtained by Group Contribution Methods or from the Equations of Wilson, NRTL, and UNIQUAC Parametrized Using Data for the Binary Systems

model	rms T/K	rms y_1	rms y_2	rms y_3
ASOG	1.22	0.0233	0.0372	0.0218
UNIFAC	0.88	0.0247	0.0372	0.0206
UNIFAC-Dortmund	0.81	0.0245	0.0438	0.0241
UNIFAC-Lyngby	1.30	0.0237	0.0355	0.0240
Wilson	0.96	0.0268	0.0394	0.0204
NRTL	1.13	0.0289	0.0417	0.0213
UNIQUAC	0.97	0.0271	0.0397	0.0205

Conclusions

Thermodynamically consistent VLE data were determined for the ternary system 1-butanol + methanol + TAME and the unmeasured constituent binary system TAME + 1-butanol. As can be seen from the ternary diagrams, Figures 1 and 2, the isotherm liquid-phase compositions close in on a single point, which corresponds to the binary azeotrope formed by the system TAME + methanol and is the focus of arrows in diagram compositions.

The Wilson, NRTL ($\alpha = 0.3$), and UNIQUAC equations correlate the ternary VLE data adequately; the deviations found in temperature and vapor composition were very similar with all three equations. When these equations were used to predict the VLE of the ternary system with binary interaction parameters obtained from the constituent binary systems, the deviations are only slightly greater than those afforded by direct optimization of the parameters of the ternary equations. This fact is attributable to the optimized parameters of the ternary and binary systems, generally being of the same order of magnitude, and to the correlation of the only system that is exceptional in this respect, methanol + 1-butanol, which is very insensitive to changes in the parameter values. This is the same behavior as has been found in previous works.^{1–2}

For this ternary system, predictions using group contribution methods present deviations in composition and temperature similar to those found when the prediction is carried out with correlation equations; nonetheless, UNIFAC (without modifications) can be selected as the best method of prediction for VLE data of the 1-butanol + methanol + TAME system.

Literature Cited

- Arce, A.; Rodil, E.; Soto, A. Extractive Distillation of 2-Methoxy-2-methylpropane + Ethanol Using 1-Butanol as Entrainer: Equilibria and Simulation. *Can. J. Chem. Eng.* **1999**, *77*, 1135–1140.
- Arce, A.; Martínez-Ageitos, J.; Rodil, E.; Soto, A. Phase equilibria involved in extractive distillation of 2-Methoxy-2-Methylpropane + Methanol using 1-Butanol as entrainer. *Fluid Phase Equilib.*, in press.
- Wilson, G. M. Vapor-Liquid Equilibrium. XI. A New Expression for the Excess Free Energy of Mixing. *J. Am. Chem. Soc.* **1964**, *86*, 127–130.
- Renon, H.; Prausnitz, J. M. Local Compositions in Thermodynamic Excess Functions for Liquid Mixtures. *AIChE J.* **1968**, *14*, 135–144.
- Abrams, D. S.; Prausnitz, J. M. Statistical Thermodynamics of Liquid Mixtures: A New Expression for the Excess Gibbs Energy of Partly or Completely Miscible Systems. *AIChE J.* **1975**, *21*, 116–118.
- Kojima, K.; Tochigi, K. *Prediction of Vapor-Liquid Equilibria by the ASOG Method*; Elsevier: Tokyo, 1979.
- Tochigi, K.; Tiegs, D.; Gmehling, J.; Kojima, K. Determination of New ASOG Parameters. *J. Chem. Eng. Jpn.* **1990**, *23*, 453–463.
- Fredenslund, A.; Gmehling, J.; Rasmussen, P. *Vapor-Liquid Equilibria using UNIFAC: A Group-Contributions Method*; Elsevier: Amsterdam, 1977.
- Weidlich, U.; Gmehling, J. A Modified UNIFAC Model. I. Prediction of VLE, h° , and γ° . *Ind. Eng. Chem. Res.* **1987**, *26*, 1372–1381.
- Gmehling, J.; Li, J.; Schiller, M. A Modified UNIFAC Model 2. Present Parameter Matrix and Results for Different Thermodynamic Properties. *Ind. Eng. Chem. Res.* **1993**, *32*, 178–193.
- Larsen, B. L.; Rasmussen, P.; Fredenslund, A. A Modified UNIFAC Group Contribution Model for Prediction of Phase Equilibria and Heats of Mixing. *Ind. Eng. Chem. Res.* **1987**, *26*, 2274–2286.
- Riddick, J. A.; Bunger, W. B.; Sakano, T. *Organic Solvents*, 4th ed.; John Wiley: New York, 1986.
- Linek, J. Excess volumes and refractive indices in benzene–tert-amyl methyl ether and cyclohexane–tert-amyl methyl ether systems at 298.15 K. *Collect. Czech. Chem. Commun.* **1987**, *52*, 2839–2843.
- Krähenbühl, M. A.; Gmehling, J. Vapor Pressures of Methyl tert-Butyl Ether, Ethyl tert-Butyl Ether, Isopropyl tert-Butyl Ether, tert-Amyl Methyl Ether and tert-Amyl Ethyl Ether. *J. Chem. Eng. Data* **1994**, *39*, 759–762.
- Arce, A.; Rodil, E.; Soto, A. Property Changes of Mixing for 1-Butanol + Methanol + 2-Methoxy-2-Methylbutane System at 298.15 K and Atmospheric Pressure. *J. Solution Chem.*, in press.
- Arce, A.; Martínez-Ageitos, J.; Rodil, E.; Soto, A. VLE measurements of binary mixtures of methanol, ethanol, 2-methoxy-2-methyl propane and 2-methoxy-2-methyl butane at 101.32 kPa. *J. Chem. Eng. Data* **1996**, *41*, 718–723.
- Wisniak, J. A New Test for the Thermodynamic Consistency of Vapor-Liquid Equilibrium. *Ind. Eng. Chem. Res.* **1993**, *32*, 1531–1533.
- Wisniak, J.; Tamir, A. Vapor-Liquid Equilibria in the Ternary Systems Water-Formic Acid-Acetic Acid and Water-Acetic Acid-Propionic Acid. *J. Chem. Eng. Data* **1977**,
- McDermott, C.; Ellis, S. R. M. A Multicomponent Consistency Test. *Chem. Eng. Sci.* **1965**, *20*, 293–296.
- Gmehling, J.; Rasmussen, P.; Fredenslund, A. Vapor-Liquid Equilibria by UNIFAC Group Contribution. Revision and Extension. 2. *Ind. Eng. Chem. Process Des. Dev.* **1982**, *21*, 118–127.

Received for review January 24, 2000. Accepted August 17, 2000.

JE000027Y